#### -- Lab 1 --

#### Rain fall data analysis

Rain fall data analysis need in many application especially in design and planning of soil and water conservation structures .

### **Basic definition :**

| Rainfall depth (mm)       | : Total rainfall accumulated at a point during storm .  |
|---------------------------|---|
| Rainfall intensity (mm\h) | : The rate at rain is falling at any storm instant.     |
| <b>Return period</b> (yr) | : Probable accurence of storm of specified depth and or |
|                           | intensity.  |

### **Type of gauges** :

 $1 - \text{simple rain gauges} \setminus \text{gives only rainfall depth}$ .

2 -recorder rain gauges \ gives rainfall depth and time of rain storm .

| Tim   | Tim interval<br>(Min) | Rainfall depth<br>(mm) | Intensity<br><mark>mm∖h</mark> |
|-------|-----------------------|------------------------|--------------------------------|
| 14:30 | 0                     | 0                      | 0                              |
| 14:35 | 5                     | 0.5                    | 6                              |
| 16:00 | 85                    | 0                      | 0                              |
| 16:30 | <mark>30</mark>       | 0.4                    | 0.8                            |
| 17:05 | 35                    | 0.9                    | 1.54                           |
| 17:10 | 5                     | 2                      | 24                             |
| 17:40 | <mark>30</mark>       | <mark>6</mark>         | <mark>12</mark>                |
| 18:55 | 75                    | 0.8                    | 0.64                           |
|       | 265 min               | 10.3 mm                |                                |

# Ex. of rainfall data analysis

\

Column 1  $\$  from the chart of rain gauge .

Column 2 \ extracted from column 1 ( first – second time ) and second ... Column 3 \ also from the chart of rain gauge .

Column 4  $\land$  from the following equation : I = column 3  $\land$  column 2 \*60

Im = Maximum intensity = 24 mm\h Total time of storm (min) = 265 min =4.41 Total rainfall depth = 10.3 mm I 30 = maximum intensity at 30 mine mm\h = 12

| No | Time (min)<br>Acumelative | Rainfull<br>depth<br>(mm)<br>Acumlative | Time<br>interval | Rainfall<br>depth | Intensity<br>Mm/hr |
|----|---------------------------|---|------------------|-------------------|--------------------|
| ١  | 0                         | 0                                       | ٠                | •                 |                    |
| ۲  | 12                        | 5                                       |                  |                   |                    |
| ٣  | 42                        | 11                                      |                  |                   |                    |
| ٤  | 70                        | 25                                      |                  |                   |                    |
| ٥  | 100                       | 35                                      |                  |                   |                    |
| ٦  | 130                       | 40                                      |                  |                   |                    |

### Calculate

Im , Total time of storm (min), Total rainfall depth , I 30

Intensity = (rainfull depth mm / time interval mm )\* 60 = .....h

# -- Lab 2 --Soil and water conservation

# The rational method

The rational method is simple and theoretically sound method for peak runoff analysis . The equation presented here may be use in design of soil and water conservation structures in watershed of less than 1000 ( Ha ) .

Peak runoff rate is determined from :

q = 0.0028CiA....(1)

where  $q = design peak runoff rate m^3 / s$ 

C = runoff coefficient

i = rainfall intensity for the design return period and for a duration

equal to the time of concentration of the watershed  $mm \setminus h$ .

A = watershed area (Ha)

Time of concentration (Tc) : the time required for water to flow from the most

remote point of the watershed to the outlet point .

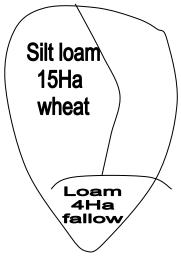
$$Tc = 0.0195L^{0.77} * S^{-0.385}$$
 .....(2)

Where Tc = time of concentration in min .

L = max. length of flow (m).

S = average watershed gradient.

The runoff coefficient (C) is the ratio of peak runoff rate to the rainfall intensity . Enclosed are 3 tables needed to estimate( c). In the first table soils are classified into 4 groups depending on their runoff producting potential .The second table Lists c values for different cropping systems and rainfall rate for soil group B. The third table correct these values for other soil groups . Ex. : The 100 yr — 6hr in Mosul is 90 mm . Determine the design peak runoff rate



for the following watershed :

Maximum distante ( L ) = 1100 m Average slope = 10 %

| 0                                  |                    | RUNOFF                 |           |                         |            |          |                                       | In the set one read   | RAT                                   | IONAL METHOD       | n sha     |         |                          |
|------------------------------------|--------------------|------------------------|-----------|-------------------------|------------|----------|---------------------------------------|---|---------------------------------------|--------------------|-----------|---------|--------------------------|
| able 4.2 Hyd                       | ologic Soil Group  | Conversion Facto       | rs        |                         |            |          | i i i i i i i i i i i i i i i i i i i | Table 4.3 (Continue   | d)                                    |                    |           |         |                          |
|                                    |                    | Factors for conv       | -         | e runoff c              | oefficie   | nt C     |                                       | Land Use  | Treatment                             | Hydrologic         | *Hyd      | drologi | c Soil Gro               |
| Courseand                          | hydrologic         |                        |           | 3 soils to <sup>u</sup> |            |          | Print                                 | or Cover  | or Practice                           | Condition          | A         | В       | С                        |
|                                    | lition             | Group A                | Group     | C                       | Group      | D        |                                       | Meadow<br>(permanent)   |                                       | Good               | 30        | 58      | 71                       |
| Row crop, p                        | oor practice       | 0.89                   | 1.09      |                         | 1.12       |          |                                       | Woods   |                                       | Poor               | 45        | 66      | 77                       |
| Row crop, G                        | ood practice       | 0.86                   | 1.09      |                         | 1.14       |          |                                       | (farm wood-   |                                       | Fair               | 36        | 60      | 73                       |
| Small grain,                       | poor practice      | 0.86                   | 1.1       |                         | 1.16       |          |                                       | lots)   |                                       | Good               | 25 '      | 55      | 70                       |
| Small grain,                       | good practice      | 0.84                   | 1.1       |                         | 1.16       |          |                                       | Farmsteads  |                                       |                    | 59        | 74      | 82                       |
| Meadow, rol                        |                    | 0.81                   | 1.1.      |                         | 1.18       |          |                                       | Roads and   |                                       | finant the         | 74        | 84      | 90                       |
| Pasture, per                       | manent, good       | 0.64                   | 1.2       |                         | 1.3        |          | and the second                        | right-of-way  |                                       |                    |           |         |                          |
| the second second                  | nature, good       | 0.45                   | 1.2       |                         | 1.40       | -        |                                       | (hard surface)  |                                       |                    |           |         |                          |
| " Factors were c<br>the curve numb | omputed from Table | 4.3 by dividing the c  | urve numb | per for the d           | lesired so | oil grou | ,                                     | *Soil Group   | Desc                                  | ription            |           |         | inal infiltr<br>Rate (mm |
| r the curve nume                   | ici ici Broup m    | 6                      |           |                         |            |          | 19.1.1                                |   |                                       |                    |           | 11.12   |                          |
| 2)                                 |                    |                        |           |                         |            |          |                                       |   | Runoff Potential<br>tle silt and clay |                    |           |         | 8-12                     |
|                                    |                    | rs for Hydrologic      |           | ver Compl               | lexes fo   | or Ante  | -                                     | meable  | loess.                                |                    |           |         |                          |
| ced                                | ent Rainfall Condi | tion II, and $I_a = 0$ | .25       |                         |            |          |                                       | B Modera  | tely Low Runof                        | F Potential. Mo    | stly san  | dy      | 4-8                      |
|                                    |                    |                        | 1         |                         |            | 8        |                                       | soils le  | s deep than A.                        | and loess less d   | eep or le | 55      |                          |
| I and I for                        | Treatment          | Hydrologic             | *H)       | drologic S              | Soil Gro   | oup      |                                       | aggrega   | ted than A, out                       | the group as a     | whole h   | as      |                          |
| Land Use                           |                    |                        | A         | В                       | С          | D        |                                       | above-a   | verage infiltratio                    | on after thoroug   | h wetting | g.      |                          |
| or Cover                           | or Practice        | Conattion              | Α         | D                       | · ·        | -        |                                       | C Modera  | tely High Run                         | off Potential.     | Compris   | cs      | 1-4                      |
| Fallow                             | Straight rov       | v                      | 77        | 86                      | 91         | 94       |                                       | shallow   | soils and soils co                    | ontaining consid   | erable cl | ay      |                          |
| Row crops                          | Straight ro        |                        | 72        | 81                      | 88         | 91       |                                       | and col   | loids, though les                     | ss than those o    | f group   | D.      |                          |
| Row crops                          | Straight ro        |                        | 67        | 78                      | 85         | 89       |                                       | The gro   | up has below-av                       | erage infiltration | n after p | re-     |                          |
|                                    | Contoured          | Poor                   | 70        | 79                      | 84         | 88       |                                       | saturati  | on.                                   |                    |           |         |                          |
|                                    | Contoured          | Good                   | 65        | 75                      | 82         | 86       |                                       | D Highes  | <b>Runoff</b> Potentia                | I. Includes mos    | tly clays | of      | 0-1                      |
|                                    | Terraced           | Poor *                 | 66        | 74                      | 80         | 82       |                                       | high sw   | elling percent, b                     | ut the group als   | so includ | les     |                          |
|                                    |                    | Good                   | 62        | 71                      | 78         | 81       |                                       |   | hallow soils with                     |                    |           |         |                          |
|                                    | Terraced           |                        | 65        | 76                      | 84         | 88       |                                       |   | s near the surfac                     |                    |           |         |                          |
| Small grain                        | Straight ro        |                        | 63        | 75                      | 83         | 87       |                                       |   |                                       |                    |           |         |                          |
|                                    | Straight ro        |                        | 63        | 74                      | 82         | 85       |                                       | Source: U. S. Soil Cons   | ervation Service, N                   | ational Engineer   | ing Hand  | book, H | lydrology,               |
|                                    | Contoured          | Poor                   |           | 73                      | 81         | 84       |                                       | (1972) and U. S. Dept. /  | gr. ARS 41-172 (1                     | 970).              |           |         |                          |
|                                    | Contoured          | Good                   | 61        | 13                      | 01         | 04       | 52 ).                                 | -   |                                       |                    |           |         |                          |
|                                    | - 1                |                        | -         |                         | -          | -        |                                       | - in the second | -                                     |                    |           |         |                          |
|                                    | T                  | able 4.1 R             | unoff     | Coeffi                  | cient      | "C       | for Agricul                           | tural Watershe  | ds (Soil Gr                           | oup B)             |           |         |                          |
|                                    |                    | Cover and              | hydro     | ologic                  | -          |          | Coefj                                 | ficient C for rainf   | all rates of                          |                    | _         |         |                          |
|                                    |                    | Con                    | dition    |                         | (I=        | 25 n     | m/h(l iph)                            | 100 mm/h (4 ip  | h) 200 r                              | nm/h (8 iph        | 10        | ~       |                          |
|                                    | وملعفط             | Row crop, p            | oor pr    | actice                  | 19-        |          | 0.63                                  | 0.65  | 11                                    | 0.66               |           |         |                          |
|                                    | - 1                | Row crop, g            |           |                         |            |          | 0.47                                  | 0.56  |                                       | 0.62               |           |         |                          |
|                                    | end,               | Small grain,           |           |                         |            |          | 0.38                                  | 0.38  |                                       | 0.38               |           |         |                          |
|                                    | - dia              | Small grain,           |           |                         |            |          | 0.18                                  | 0.21  |                                       | 0.38               |           |         |                          |
|                                    | فالناية            | Meadow, rot            | ation     | good                    | -          |          | 0.29                                  |   |                                       |                    |           |         |                          |
|                                    | celi               | Pasture, per           | mones.    | tagad                   |            |          |                                       | 0.36  |                                       | 0.39               |           |         |                          |
|                                    |                    | rasture, per           | nanen     | r, good                 |            |          | 0.02                                  | 0.17  |                                       | 0.23               |           |         |                          |
|                                    | 241                | Woodland, n            | notres    |                         |            |          | 0.02 .                                | 0.10  |                                       | 0.15               |           |         |                          |

### -- Lab 3 --Direct runoff analysis

Data from gauged watersheds in the U.S showed the following basic relationship between rainfall and runoff :

Where **P** = Precipitation from the storm being analyzed .

Ia = Precipitation abstraction .

Q = Total runoff.

 $\mathbf{S}=\mathbf{Max.}$  potential difference between P and Q at the beginning of the storm .

**Equation 1 may be written as :** 

Q = 
$$\frac{(P - Ia)^2}{P - Ia + S}$$
 .....(2)

Data also showed that :

Hence :

$$Q = \frac{(P - 0.2 S)^2}{P + 0.8 S}$$
 (4)

For convenience, an orbitrary quantity called curve number " CN " was chosen such that :

$$CN = \frac{25400}{S + 254} - \dots - (5)$$

Where S is measured in ( mm )

When  $S \rightarrow \%$ ,  $CN \rightarrow 0$  which means there is no runoff.

When  $S \rightarrow 0$ ,  $CN \rightarrow \%$  and all rainfall becomes runoff in an ideal situation .

### Selection of a curve number (CN)

The  $1^{st}$  watershed factor affecting CN is soil type . Soils varies from group A with the lowest runoff potential to group D with the highest runoff potential .

The 2<sup>nd</sup> factor is the antecedent soil moisture condition or AMC.

AMC is classified as follow :

AMC – I : Soils are dry but moisture is above the wilting point .

AMC – II : Average condition usually precedes the occurrence of the max.

annual flood .

- AMC III : Soils are nearly saturated .
- EX . The 50 yr 24 h storm in Mosul is 80 mm . Calculate total runoff for the three conditions of soil moisture . Mosul soil is clay loam .

. . .

(assuming good pasture).

| Curve Number        | Factor to Conve<br>for Cond | ert Curve Number<br>dition II to |
|---------------------|-----------------------------|----------------------------------|
| for<br>Condition II | Condition I                 | Condition III                    |
| 10                  | 0.40                        | 2.22                             |
| 20                  | 0.45                        | 1.85                             |
| 30                  | 0.50                        | 1.67                             |
| 40                  | 0.55                        | 1.50                             |
| 50                  | 0.62                        | 1.40                             |
| 60                  | 0.67                        | 1.30                             |
| 70                  | 0.73                        | 1.21                             |
| 80                  | 0.79                        | 1.14                             |
| 90                  | 0.87                        | 1.07                             |
| 100                 | 1.00                        | 1.00                             |

| internet             |  | "Hydrologic Soil Grou,                          | C  | 11              | 1           | 1     | 02        | 82          | 06          |                                | Final infiltrat  | Rate (mmil                       | 8-12  | 4-8  | 0  | 1-4   |  |   | 0-1  |  |   |                      | Hydrology, Se        |                                  |                      |          | that: (1) ri   | e time of co  | intensity ov.   | d, the rainfa   | y Fig. 4.3a  | al to the ti  | urred, the 1   | be less than  | ration). A r  |
|----------------------|--|---|--|-----------------|-------------|-------|-----------|-------------|-------------|--------------------------------|--|----------------------------------|---|--|--|---|--|---|--|--|---|----------------------|----------------------|----------------------------------|----------------------|----------|--|---|---|---|--|---|--|---|---|
|                      |  | Hydrolog  | B  | 58              |             |       | 55 .      |             |             |                                |  |                                  | s with  | y per-   | or less<br>ic has  | tting.<br>Drises  | e clay   | r pre-  | The set  | cludes   | e sub-  |                      | andbook.             |                                  |                      |          | mptions  | ual to th   | uniform   | re fulfille   | hically t  | tion equ  | n Te occ   | y would   | / and du  |
| 201                  |  |   | A 10   | 30              |             | 45    | 25        | 65          | 74          |                                |  |                                  | leep sand   | p, rapidij<br>Moetlo   | ss deep o  | rough wel   | nsiderabl  | ation afte  | In other   | p also inc   | permeable                                       |                      | neering H            |                                  |                      |          | the assu   | least equ   | irs at a t  | ions wer  | ted grap   | r a dura  | eater tha  | intensity   | intensity   |
| KALIUNAL MELTUU      |  | Hydrologic                                      | Condition  | Good            |             | Poor  | Good      | 1           | 1           |                                |  | ption                            | Includes d  | also dec   | d loess le   | after thor  | taining co   | age infiltr   | Indudae  | t the grou   | nearly imp                                      |                      | tional Engi          | .(0)                             |                      |          | d from 1   | ration at   | nfall occi  | assumpt   | represen   | ensity for  | ation gre  | e rainfall  | I rainfall  |
| NIN                  | (þe  | Treatment                                       | or Practice                                      |                 |             |       |           |             |             |                                | Color I  | Description                      | Lowest Runoff Potential. Includes deep sands with | very little stit and clay, also deep, rapidly per-<br>meable loess.  | solis less deep than A, and loess less deep or less<br>aggregated than A, but the group as a whole has | above-average infiltration after thorough wetting.<br>Moderately High Runoff Potential. Comprises | shallow soils and soils containing considerable clay | The group has below-average infiltration after pre- | saturation.<br>Unitere Decode Potantial Includes mostly class of | high swelling percent, but the group also includes | some shallow soils with nearly impermeable sub- | IS BEAF UP SUITAGE   | ervation Service, Na | S. Dept. Agr. ARS 41-172 (1970). |                      |          | The rational method is developed from the assumptions that: (1) ri | ntensity for a du   | rshed, and (2) rai  | atershed. If these  | ershed would be  | n of uniform inte   | If a storm of dur  | than q because th   | ionships between  |
| The second           | Table 4.3 (Continued)                              | Land Use  | or Cover   | Meadow          | (permanent) | Woods | lots)     | Farmsteads  | Roads and   | right-of-way<br>(hard surface) |  | *Soil Group                      | A Lowest  | meable<br>meable   |  | C Moder   |  | The gr  | D Biohast D  |  | some s  | 0711011              |                      | 1972) and U. S. Dept.            |                      |          | The rational me  | occurs at uniform intensity for a duration at least equal to the time of co | tration of the watershed, and (2) rainfall occurs at a uniform intensity ov | entire area of the watershed. If these assumptions were fulfilled, the rainfa | runoff for the watershed would be represented graphically by Fig. 4.3a | figure shows a rain of uniform intensity for a duration equal to the ti | concentration, $T_c$ . If a storm of duration greater than $T_c$ occurred, the 1 | rate would be less than q because the rainfall intensity would be less than | Chapter 2 for relationships between rainfall intensity and duration). A r |
|                      |  |   |  |                 |             |       |           |             |             |                                |  |                                  |   |  |  |   |  |   |  | _  | 1.  | _                    |                      |                                  | -                    | _        |  | 1   |   |   |  |   |  |   |   |
|                      | -  | 1.4.  | 4.   |                 |             |       |           |             |             | N.                             | -  |                                  | -ti-  |  |  |   |  |   |  |  |   |                      |                      |                                  |                      |          |  |   |   |   |  |   |  |   |   |
|                      |  | nt C  | - W.   | D .             |             |       | 5         | 9           | 8           |                                | oil group  |                                  |   | or Ante-   | dne  | D   | 54   | 89  | 88   | 8 58   | 18  | 88                   | 85                   | 84                               | 82                   | 68       | 85   | 85  | 63  | 80  | 68   | 84  | 88   | 83  | 62  |
| in the second second |  | Coefficient C                                   | o"   | Group D         | 117         | 1.14  | 1.16      | 1.16        | 1.18        | 1.31                           | e desired soil group   |                                  | •   | plexes for Ante-   | c Soil Group   | c D   |  |   | 84 88  |  |   |                      |                      |                                  | 79 82                |          |  |   |   |   | 86 89  |   |  | 75 83   |   |
|                      |  | the runoff coefficient C                        | B soils to"                                      |                 |             |       |           | -           | -           |                                | nber for the desired soil group  |                                  |   | over Complexes for Ante-   | Hydrologic Soil Group  |   |  | 85  | 2  |  | 78  | ¥ 8                  | 8.8                  | 18                               | 2.2                  | 88       | 72 81  | 75 83   | 6/ 60<br>8/   | 67 76   | 79 86  | 66 69   | 61 14<br>67 81   | 59 75   | 70  |
| 1                    | tors   | nvertive the runoff coefficient C               | on group B soils to"                             | Group C Group D | c1 1 00 1   |       |           | -           | -           |                                | curve number for the desired soil group  |                                  | •   | ic Soil-Cover Complexes for Ante-<br>0.25  | *Hydrologic Soil Group   | A B C   | 16   | 78 85   | 79 84  | 2 8  | 71 78   | 76 84                | 74 82                | 73 81                            | 2.2                  | 77 85    | 72 81  | 75 83   | 6/ 60<br>8/   | 76  | 79 86  | 66 69   | 61 14<br>67 81   | 59 75   | 35 70   |
|                      | mversion Factors                                   | actors for convertise the runoff coefficient C  | actors for converting the rating coefficients of |                 | 1.00        |       | 111       | 1.11 1      | 1.13        |                                | by dividing the curve number for the desired soil group  |                                  |   | for Hydrologic Soil-Cover Complexes for Ante-<br>n II. and L = 0.25  |  | A B C   | 77 86 91   | 78 85   | 70 79 84   | 28 CI<br>17 80                                     | 1 62 71 78                                      | 65 76 84<br>22 76 84 | 74 82                | 1 61 73 81                       | 61 72 19<br>60 70 76 | 77 85    | 1 58 72 81   | 64 75 83  | 0/ 60 CC  | 67 76   | 68 79 86   | 49 69 79  | 61 14<br>67 81   | 25 59 75  | 4 K 70  |
| · curcinet           | Table 4.2 Hydrologic Soil Group Conversion Factors | Factors for converting the ranoff coefficient C | -  | Group C         | 00.1 00.0   | 1.09  | 0.86 1.11 | 0.84 1.11 1 | 0.81 1.13 1 | d 0.64 1.21 1<br>0.45 1.27 1   | <ul> <li>Factors were computed from Table 4.3 by dividing the curve number for the desired soil group</li> </ul> | by the curve number for group B. |   | Runoff Curve Numbers for Hydrologic Soil-Cover Complexes for Ante-<br>cedent Rainfall Condition II. and L = 0.25 |  | Condition A B C   | 16 98 22 -   | 67 78 85  | Poor 70 79 84  | 56 C1 C0   | Good 62 71 78                                   | Poor 65 76 84        | 63 74 82             | Good 61 73 81                    | Poor 61 72 79        | 66 77 85 | Good 58 72 81  | Poor 64 75 83   | d Good 33 69 78   | 51 67 76  | Poor 68 79 86  | 49 69 79  | Gopd 39 61 /4<br>Door 47 67 81   | 25 59 75  | Good 6 15 70  |

#### -Lab 4-

Soil and water conservation planning needs an estimate for the amount of erosion occuring in the field . The mathematical formula used to predict erosion are called *MODEL*.

The most common water erosion model is the Universal Soil Loss Equation (USLE) which covers all geographic region and can be applied in addition to agricultural field areas to estimate the soil loss from cultivated, forest, and range lands using the following formula :

A = R \* K \* L \* S \* C \* P.

Where :

A = Mean annual soil loss t / ha. / yr

R= Rainfall – runoff erosivity factor.

K = Soil erodibility factor

- L = Slope length factor.
- S= Slope steepness factor.
- C= cropping system and soil management factor.
- P = Supporting practices factor. 2

Threefore ,we can use the Universal Soil Loss Equation (USLE) to predicts the long-term average annual rate of water erosion (A) on a field slope based on rainfall pattern (R), soil type (K), topography factor (LS), crop system and management practices (C) with supporting engineering practices factor (P).

#### -Lab 5-

#### **Rainfall – runoff erosivity factor**

#### R

The simplist method used to estimate the R-factor is using the modified Fourneir Index model, which expressed by the following formula:

$$R = 0.0302 (------)^{1.93}$$

R = Rainfall - runoff erosivity factor.

Pi = Average monthly rainfall depth ( mm ).

P = Average annual rainfall depth ( mm ).

n = number of rainy months

Ex: Calculte the rainfall erosivity factor ( R ) for Mosul city during the following rainy months were :

| Month          | Oct. | Nov. | Dec. | Jan. | Feb. | Mar. | Apr. | May |
|----------------|------|------|------|------|------|------|------|-----|
| Rainstorm (mm) | 10   | 18   | 20   | 20   | 40   | 25   | 10   | 5   |

$$R = 0.0302 \ \left( \begin{array}{c} \frac{\Sigma^{n} \quad Pi^{2}}{P} \end{array} \right)^{1.93}$$

$$R = 0.0302 \ \left( \begin{array}{c} \frac{10^{2} + 18^{2} + \ 20^{2} + 20^{2} + 40^{2} + 25^{2} + 10^{2} + 5^{2}}{10 + 18 + 20 + 20 + 40 + 25 + 10 + 5} \right)^{1.93}$$

$$R = 0.0302 \left( \begin{array}{c} 3573 \\ ------ \\ 148 \end{array} \right)^{1.93}$$

$$R = 0.0302 (24.15)^{1.93}$$

- R = 0.0302 \* 461.1
- R = 13.92 metric unit

## -Lab 6-

## Soil Erodibility Factor factor

#### Κ

Soil Erodibility (K - factor) in the Universal Soil Loss Equation (USLE) represents the susceptibility of the soil to the erosion process. The soil erodibility factor (K), which depends on properties involved

1- Particle size distribution of ( % Sand ,% very fine sand , and % silt )

2- % Soil organic matter

3- Soil structure

4- Soil permeability

All the above soil properties were collected in to special curves called erodibility - nomgraph which was published by Wischmeier and Smith (1978)

From this nomograph we can conludede that the soil erodibility depend mainly on the three soil physical proerties (texture, structure and permeability) with one soil chemical (% organic matter). Many studies showed that the soil texture is the main factor which dtermined the suspility of soil to water erosion. The following table lists the values of K-factor from the fine soil texture (higher erodibility) to more coarser textures soils (lower erodibility).

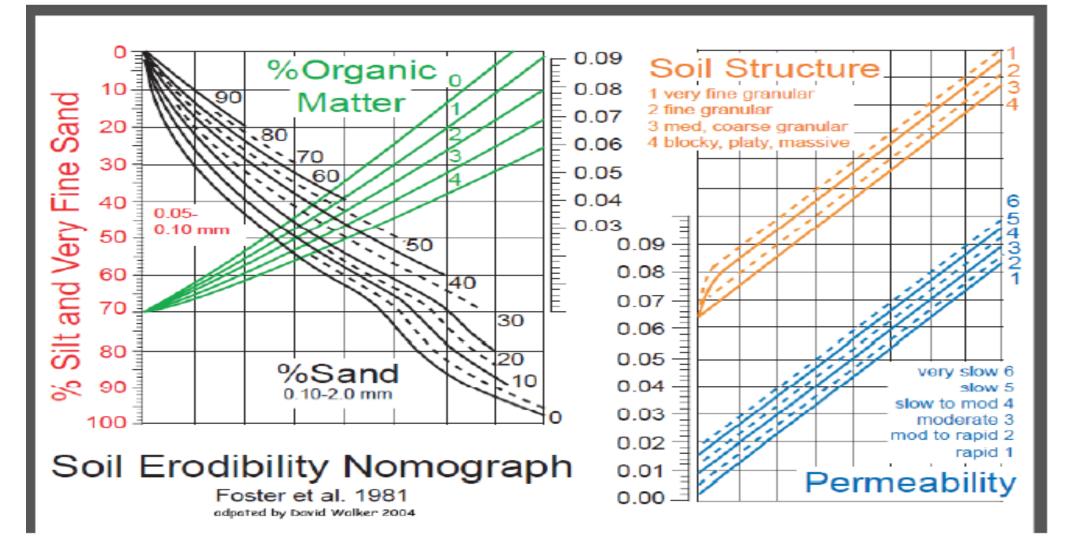


Fig ( ): Nomograph for k-factor calculation

## -- Lab 7 --The Topographic Factor

The Topographic Factor includes the effect of slope length and slope gradient .

Slope length : The distance from the point of origin of over land flow to the point the point ether the slope gradient decreases enough that deposition begins , or the runoff water enters a well defined channel .
Slope gradient : The sine of the slope angle .
Uniform slope : The slope of nearly constant gradient .

LS factor is estimated from :

Where  $\lambda = \text{slope length}(m)$ .

 $\Theta$  = angle of slope.

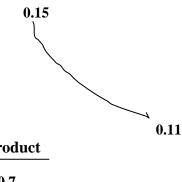
m = 0.5 if the percent slope is 5 or more , 0.4 on slope of 3.5 to 4.5 percent , 0.3 on slope of 1 - 3 percent and 0.2 on slope of less than 1 %.

Irregular slope : many filed slopes either steep on toward the lower end (concave slope ).

The following procedure is used to obtain LS for irregular slopes :

- 1-divide the irregular slope into equal length segments . slopes of these segment is assumed uniform .
- 2- Lists the segment gradients in the order in which they accure on the slope , beginning at the upper end .
- $3-Estimate\ LS$  using the above equation for each segment . substitute total slope length for L .
- 4 Multiply LS factors in 3 by the corresponding factor from :eg . mention below
- 5 Add the values in 4 to obtain total slope length .

**Ex : Determine the LS factor for the adjacent slope:** 



| segment | slope | LS   | factor | product |
|---------|-------|------|--------|---------|
| 1       | 0.14  | 2    | 0.35   | 0.7     |
| 2       | 0.12  | 1.56 | 0.65   | 1       |
|         |       |      |        | 1.7     |

ملاحظة / يتخلل بين كل محاضرة وأخرى تطبيق عملي لحل المسائ