Geomechanics Classification

Rock Mass Rating System

RMR

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Rock Mass Classification System	Originator	Application Areas
Rock Load	Terzaghi, 1946	Tunnels with steel Support
Stand-up Time	Lauffer, 1958	Tunneling
New Austrian Tunneling Method (NATM)	Pacher, et al., 1964	Tunneling
Rock Quality Designation (RQD)	Deere, et al., 1967	Core logging, tunneling
Rock Classification for Rock Mechanical Purposes	Patching and Coates, 1968	For input in rock mechanics
The Unified Classification of Soils and Rocks	Deere et al., 1969	General
Rock Mass Rating (RMR)	Bieniawski, 1973	Tunnels, mines, slopes, foundations
Tunneling Quality Index (Q)	Barton, et al., 1974	Tunnels, mines, foundations
Rock Structure Rating (RSR)	Wickham, et al., 1974	Tunneling
Strength-Block Size	Franklin, 1975	Tunneling and mining
The Typological Classification	Matula and Holzer, 1978	General
Basic Geotechnical Classification	ISRM, 1981	General
Rock Mass Strength (RMS)	Stille, et al., 1982	Metal mining
Unified Rock Mass Classification System (URCS)	Williamson, 1984	General
Slope Mass Rating (SMR)	Romana, 1985	Slopes
Modified Rock Mass Rating (M-RMR)	Unal and Ozkan, 1990	Mining
Geomechanics Classification System	Laubscher, 1990	Mining
Rock Mass Index (RMi)	Palmstrom, 1995	Rock engineering
Rock Mass Number (N)	Goel, et al., 1995	Tunnels, mines, foundations
Geological Strength Index (GSI)	Hoek and Brown, 1997	All underground excavations
Geo-Engineering Classification	Ramamurthy, 2004	For intact and jointed rocks
Japanese Geotechnical Society JGS	Osada, et al., 2005	preliminary investigations
Rock Slope Stability (RSS)	Liu and Chen, 2007	Slope stability

Classification Procedure

- The following six parameters are used to classify a rock mass using the RMR system (Geomechanics Classification).
- 1.Uniaxial compressive strength of rock material.
- 2.Rock quality designation (RQD).
- 3.Spacing of discontinuities.
- 4. Condition of discontinuities.
- 5. Groundwater conditions.
- 6.Orientation of discontinuities.

To apply the RMR system, the rock mass is <u>divided into a number of structural regions</u> such that certain features are more or less uniform within each region. Although rock masses are discontinuous in nature, they may, nevertheless, be uniform in regions when, for example, the type of rock or the discontinuity spacing are the same throughout that region. In most cases, the boundaries of structural regions will coincide with major geological features such as faults, dykes, shear zones, *etc*.











A. CLASSIFICATION PARAMETERS AND THEIR RATINGS

Parameter		ameter			Ranges of Values				
,	Strength of	Point-load strength index (MPa)	>10	4-10	2-4	1-2	For this low range, unlaxial compressive test is preferred		l erred
	material	Uniaxial compressive strength (MPa)	>250	100 - 250	50 - 100	25-50	5-25	1-5	<1
		Rating	15	12	7.	4	2	1	0
2	Drill core	e quality RQD (%)	90 ~ 100	75-90	50-75	25-50		<25	
		Rating	20	17	13	8		3	
3	Spacing	of discontinuities	>2 m	0.6-2 m	200-600 mm	60~200 mm		<60 mm	
		Rating	20	15	10	8		5	
•	Condition of discontinuities		Very rough surfaces Not continuous No separation Unweathered wall rock	Slightly rough surfaces Separation < 1 mm Slightly weathered walls	Slightly rough surfaces Separation < 1 mm Highly weathered wall	Slickensided surfaces or Gouge < 5 mm thick or Separation 1 – 5 mm Continuous	Soft gouge > 5 mm thick or Separation > 5 mm Continuous		
	Rating		30	25	20	10		0	
		Inflow per 10 m tunnel length (Umin)	None	<10	10-25	25-125 or	ar	>125	
5	Groundwater	Joint water Pressure Major principal stress	0	<0.1	0.1-0.2	0.2-0.5	or	>0.5	
General conditions		General conditions	Completely dry	Damp	Wet	Dripping		Flowing	
Rating		Rating	15	10	7	4		0	

B. RATING A	DJUSTMENT FOR	DISCONTINUITY ORIE	NTATIONS (See	F)				
Strike and dip	orientations	Very favourable	Favourable		Fair	Unfavo	ourable	Very Unfavourable
	Tunnels & mines	0	-2		-5	· -	10	-12
Ratings	Foundations	0	-2		-7	-	15	-25
	Slopes	٥	-5		-25	-9	50	
C. ROCK MA	SS CLASSES DETE	RMINED FROM TOTA	L RATING\$					
Rating		100 ← 81	80 ← 61		60 ← 41	40 4	- 21	< 21
Class number	ſ					ľ	V	V
Description		Very good rock	Good rock		Fair rock	Poor	rock	Very poor rock
d. Meaning	OF ROCK CLASSE	S						
Class number	ſ	I			11	ľ	V	V
Average stan	d-up time	20 yrs for 15 m span	1 year for 10 m	span	1 week for 5 m span	10 hrs for 3	2.5 m span	30 min for 1 m span
Cohesion of r	ock mass (kPa)	> 400	300 - 400		200 - 300	100 -	- 200	< 100
Friction angle	of rock mass (deg)	> 45	35 - 45		25 - 35	15 - 25		< 15
e. Guidelin	ES FOR CLASSIFIC	ATION OF DISCONTIN	UITY conditions	8				
Discontinuity	length (persistence)	< 1 m	1 - 3 m		3 - 10 m	10 - 3	20 m	> 20 m
Rating		6	4		2		1	D
Separation (a	iperture)	None	< 0.1 mm		0.1 - 1.0 mm	1-5	mm	>5mm
Rating		6	5		4 Click durante		1	U Of all and
Roughness Rating		very rougn 6	Hough		Slightly rough	SITK	00th 1	D
Infiling (apug	<i>~</i>)	None	J Hard filling < 5	0000	J Hard filling > 5 rom	Soft filling	1 a < 5 mm	Soft filling > 5 mm
Rating	10)	6	4		2		Z	D
Weathering		Unweathered	Slightly weathe	red	Moderately	Highly w	eathered	Decomposed
Ratings		6	5		weathered		1	D.
-					3			
F. EFFECT C	F DISCONTINUITY	STRIKE AND DIP ORI	ENTATION IN TU	NNEL	LING**			
Strike perpendicular to tunnel axis					Strike	e parallel to	turnel axis	
Drive with dip - Dip 45 - 90° Drive with dip - Dip 20 - 45°		Dip 20 - 45'	Dip 45 - 90° Dip 20 - 45		ip 20 - 45°			
Ve	ry favourable	Favour	able		Very unfavourable		Fair	
Drive agai	inst dip - Dip 45-90°	Drive against dip	- Dip 20-45°	Dip 0-20 - Irrespective of strike				2 ⁰
Fair		Unfavou	rable	Fair				

Application in Tunnels Stand-Up Time X Roof Span





Example

A tunnel is to be driven through slightly weathered granite with a dominant joint set dipping at 60° against the direction of the drive. Index testing and logging of diamond drilled core give typical Point load strength index values of 8 MPa and average *RQD* values of 70%. The joints, which are slightly rough and slightly weathered with a separation of < 1 mm, are spaced at 300 mm. Tunneling conditions are anticipated to be wet. The *RMR* value is determined as follows:

Table	Item	Value	Rating
1: A.1	Point load index	8 MPa	12
1: A.2	RQD	70%	13
1: A.3	Spacing of discontinuities	300 mm	10
1: E.4	Condition of discontinuities	Note 1	22
1: A.5	Groundwater	Wet	7
1: B	Adjustment for joint orientation	Note 2	-5
		Total	59

Note 1. For slightly rough and altered discontinuity surfaces with a separation of < 1 mm, Table 1.A.4 gives a rating of 25. When more detailed information is available, Table 1.E can be used to obtain a more refined rating. Hence, in this case, the rating is the sum of: 4 (1-3 m discontinuity length), 4 (separation 0.1-1.0 mm), 3 (slightly rough), 5 (no infilling) and 5 (slightly weathered) = 21.

Slightly rough surfaces Separation < 1 mm Slightly weathered walls
25

E. GUIDELINES FOR CLASSIFICATION OF DISCONTINUITY conditions						
Discontinuity length (persistence)	<1 m	1-3 m	3 - 10 m	10 - 20 m	> 20 m	
Rating	6	4	2	1	D	
Separation (aperture)	None	≺0.1 mm	0.1 - 1.0 mm	1 - 5 mm	> 5 mm	
Rating	6	5	4	1	0	
Roughness	Very rough	Rough	Slightly rough	Smooth	Slickensided	
Rating	6	5	3	1	D	
Infiling (gouge)	None	Hard filing < 5 mm	Hard filling > 5 mm	Soft filling < 5 mm	Soft filing ≻ 5 mm	
Rating	6	4	2	2	0	
Weathering Ratings	Unweathered 5	Slightly weathered 5	Moderately weathered 3	Highly weathered 1	Decomposed D	

Note 2. Table 1.F gives a description of 'Fair' for the conditions assumed where the tunnel is to be driven against the dip of a set of joints dipping at 60°. Using this description for 'Tunnels and Mines' in Table 1.B gives an adjustment rating of -5.

F. EFFECT OF DISCONTINUITY STRIKE AND DIP ORIENTATION IN TUNNELLING**						
Strike perpendicu	lar to tunnel axis	Strike parallel to tunnel axis				
Drive with dip - Dip 45 - 90°	Drive with dip - Dip 20 - 45'	Dip 45 - 90°	Dip 20 - 45°			
Very favourable	Favourable	Very unfavourable	Fair			
Drive against dip - Dip 45-90° Drive against dip - Dip 20-45° Dip 0-20 - Irrespective of strike°						
Fair Unfavourable Fair						

B. RATING ADJUSTMENT FOR DISCONTINUITY ORIENTATIONS (See F)									
Strike and dip	Strike and dip orientations Very favourable Favourable Fair Unfavourable Very Unfavourable								
	Tunnels & mines	0	-2	-5	-10	-12			
Ratings	Foundations	٥	-2	-7	-15	-25			
	Slopes	٥	-5	-25	-50				

The value of *RMR* of 59 indicates that the rock mass is on the boundary between the 'Fair rock' and 'Good rock' categories. In the initial stages of design and construction, it is advisable to utilize the support suggested for fair rock. If the construction is progressing well with no stability problems, and the support is performing very well, then it should be possible to gradually reduce the support requirements to those indicated for a good rock mass. In addition, if the excavation is required to be stable for a short amount of time, then it is advisable to try the less expensive and extensive support suggested for good rock. However, if the rock mass surrounding the excavation is expected to undergo large mining induced stress changes, then more substantial support appropriate for fair rock should be installed. This example indicates that a great deal of judgment is needed in the application of rock mass classification to support design.

It should be noted that Table 2 has not had a major revision since 1973. In many mining and civil engineering applications, steel fiber reinforced shotcrete may be considered in place of wire mesh and shotcrete.

Rock mass class	Excavation	Rock bolts (20 mm diameter, fully grouted)	Shotcrete	Steel sets
I - Very good rock <i>RMR</i> : 81-100	Full face, 3 m advance.	Generally no support required except spot bolting.		
II - Good rock <i>RMR</i> : 61-80	Full face , 1-1.5 m advance. Complete support 20 m from face.	Locally, bolts in crown 3 m long, spaced 2.5 m with occasional wire mesh.	50 mm in crown where required.	None.
III - Fair rock <i>RMR</i> : 41-60	Top heading and bench 1.5-3 m advance in top heading. Commence support after each blast. Complete support 10 m from face.	Systematic bolts 4 m long, spaced 1.5 - 2 m in crown and walls with wire mesh in crown.	50-100 mm in crown and 30 mm in sides.	None.
IV - Poor rock <i>RMR</i> : 21-40	Top heading and bench 1.0-1.5 m advance in top heading. Install support concurrently with excavation, 10 m from face.	Systematic bolts 4-5 m long, spaced 1-1.5 m in crown and walls with wire mesh.	100-150 mm in crown and 100 mm in sides.	Light to medium ribs spaced 1.5 m where required.
V – Very poor rock <i>RMR</i> : < 20	Multiple drifts 0.5-1.5 m advance in top heading. Install support concurrently with excavation. Shotcrete as soon as possible after blasting.	Systematic bolts 5-6 m long, spaced 1-1.5 m in crown and walls with wire mesh. Bolt invert.	150-200 mm in crown, 150 mm in sides, and 50 mm on face.	Medium to heavy ribs spaced 0.75 m with steel lagging and forepoling if required. Close invert.

Modifications to *RMR* **for mining**

Originally based upon case histories drawn from civil engineering, several modifications have been proposed in order to make the classification more relevant to mining applications

Laubscher (1977, 1984), Laubscher and Taylor (1976) and Laubscher and Page (1990) Modified Rock Mass Rating system for mining MRMR. In situ and induced stresses, stress changes and the effects of blasting and weathering

> Cummings et al (1982) and Kendorski et al (1983) MBR (modified basic RMR) system

blast damage, induced stresses, structural features, distance from the cave front and size of the caving block

Homework

A mudstone rock mass at a depth of 200 m contains three fracture sets. One set comprises bedding planes; these are highly weathered, slightly rough surfaces, and are continuous with an orientation of 180/10. Another set is jointing; these joints are slightly weathered, slightly rough, and have an orientation of 185/75. The third set is also jointing; again, the joints are slightly weathered and slightly rough, and have an orientation of 090/80. The strength of the intact rock has been assessed as 55 MPa, and values for the RQD and mean fracture spacing are reported as 60% and 0.4 m, respectively. Use the RMR system to classify this rock mass, and assess the stability of a 10 m wide excavation being driven from east to west.

Thank you