

# PLAXIS 2.D

Plaxis: is a Package use a Finite Element Method (FEM) to analyze

different type of structures, such as:

- settlement of different types of foundation and stresses under foundation,
- Construction of an excavation (analysis of diaphragm wall),
- Analysis of embankment contains road embankments,
- Settlement due to tunnel construction.

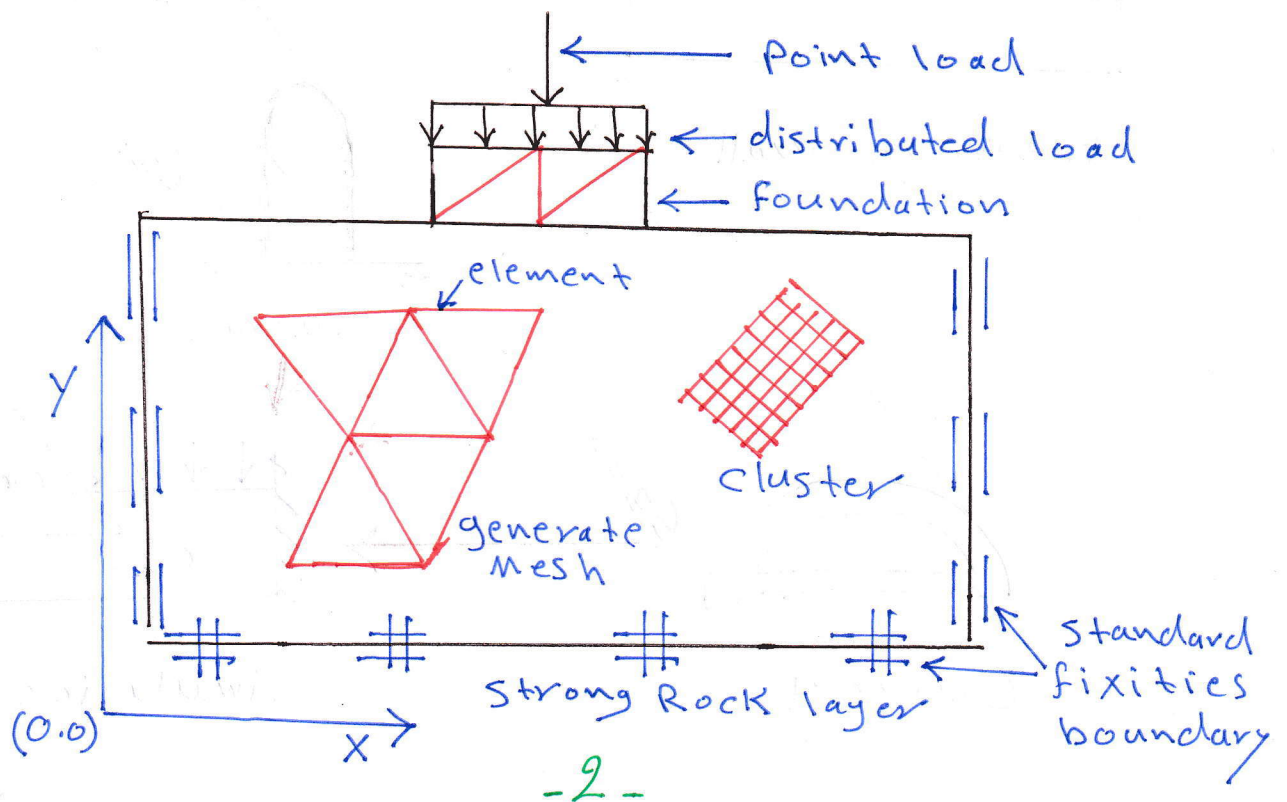
## Dynamic Analysis

- Dynamic analysis of generator on a foundation,
- Dynamic analysis of pile driving
- Dynamic analysis of building subjected to an earthquake.

The Plaxis 2.1D consists of four sub-Programs:

- Input Program
- Calculation Program
- Out put Program
- Curve Program

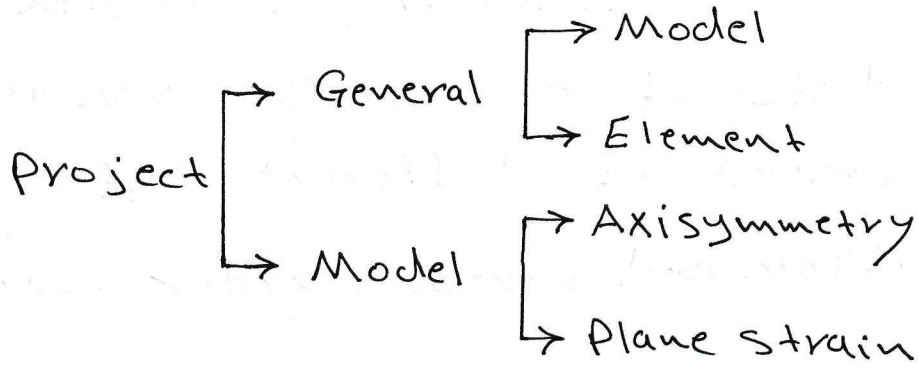
**Input Program:** The input Program contains all facilities to 1- Create and modify a geometry model, 2- generate a finite element mesh, and 3. The generation of initial condition.



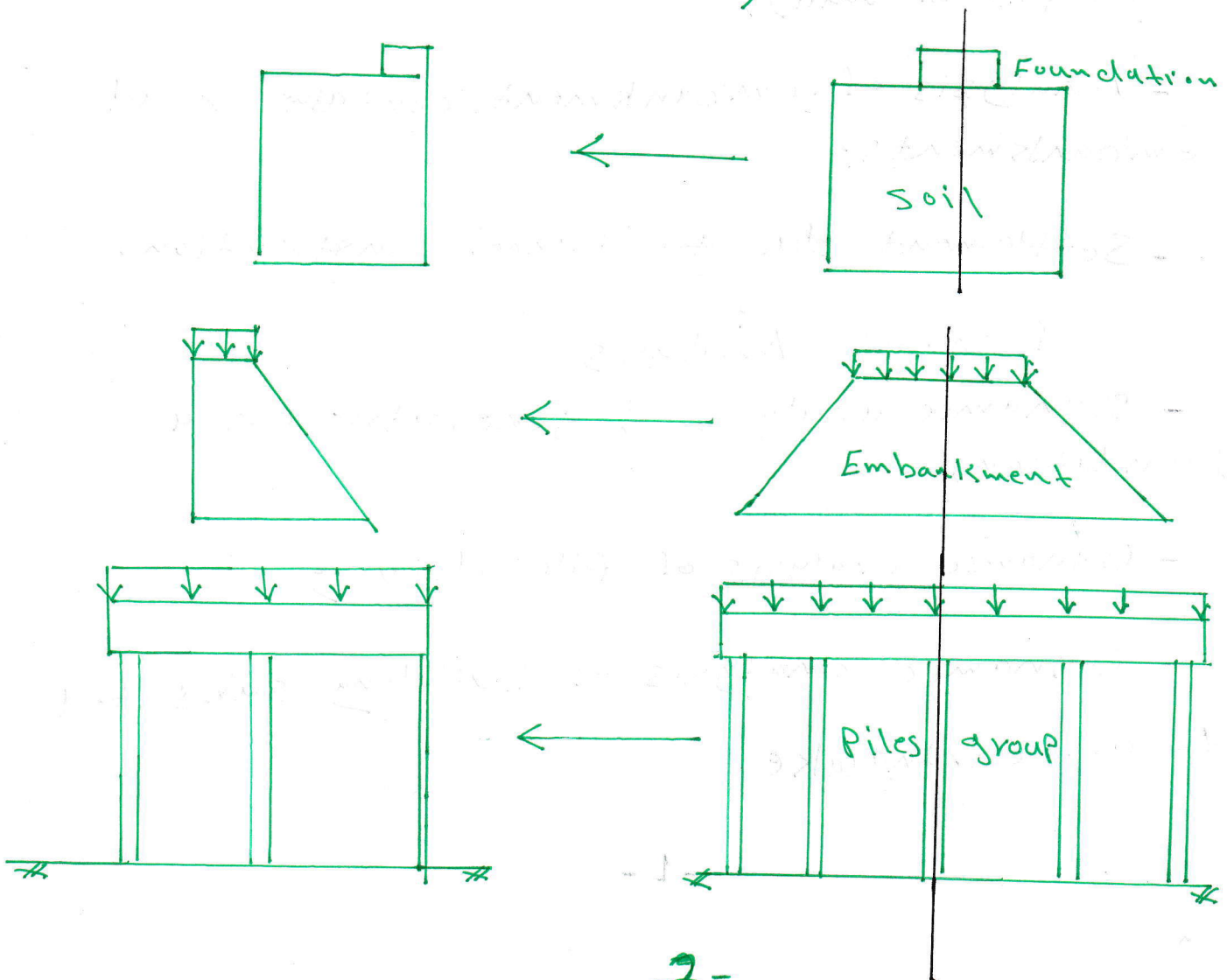
# General setting

15-21X-11

- Project
- dimension

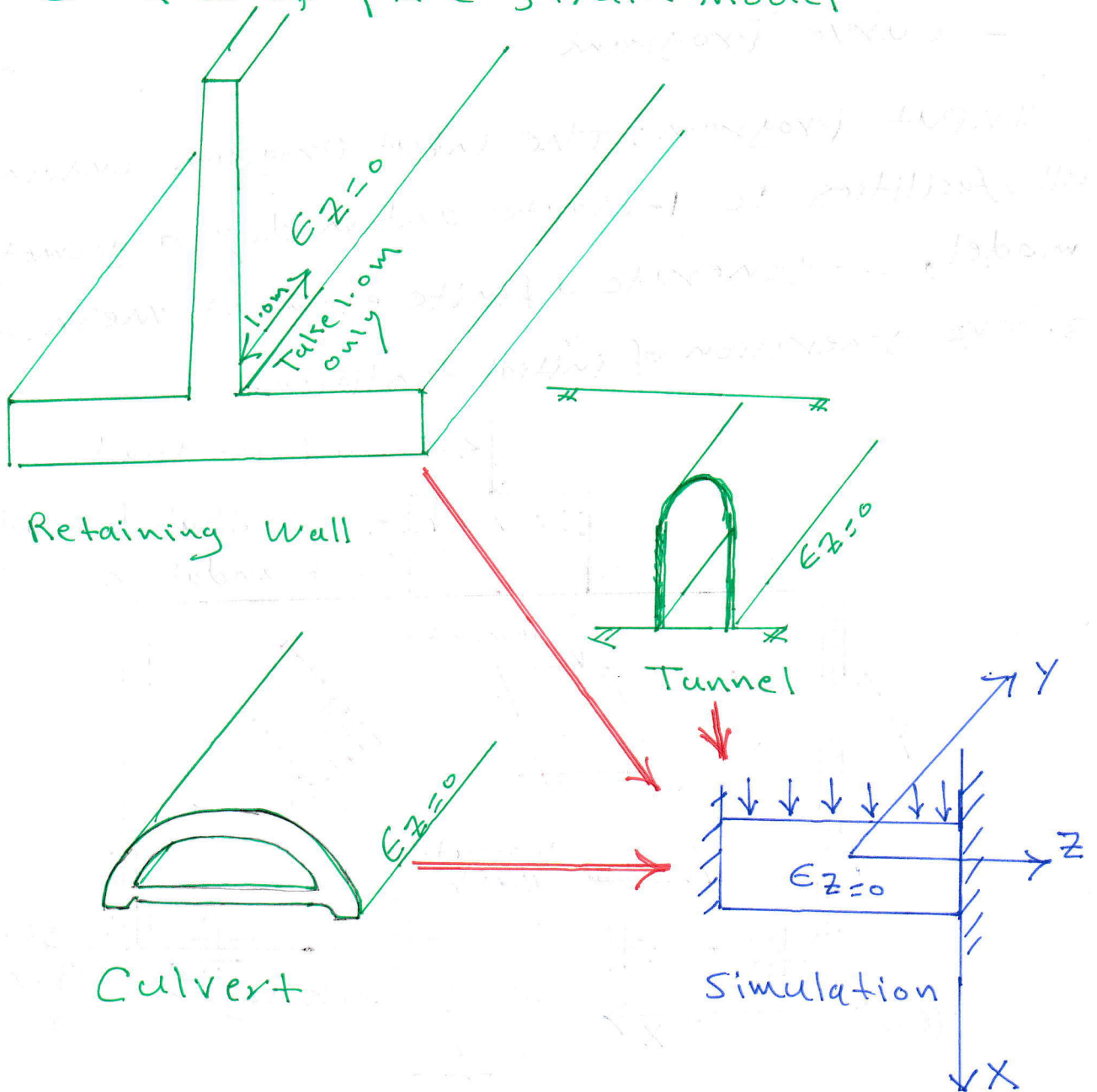


## Samples of Axisymmetry Model



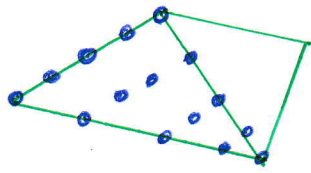
Plane Strain: Problems where the body is infinitely long ( $\epsilon_z = 0$ ). We can examine the body with 1.0 m. length

### Samples of plane strain model

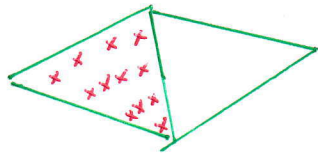


Element  $\left\{ \begin{array}{l} \rightarrow 15 \text{ node element} \\ \rightarrow 6 \text{ node element} \end{array} \right.$

15. node element



15-node element

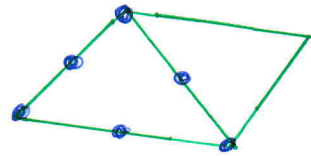


Stress (Gaussian element)

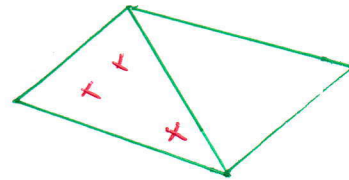
- A 15-node element is more accurate for displacement calculation ( $U_x, U_y$ )

- 15-node element gives (12-stress element) for stress calculation.

6. node element



6-node element



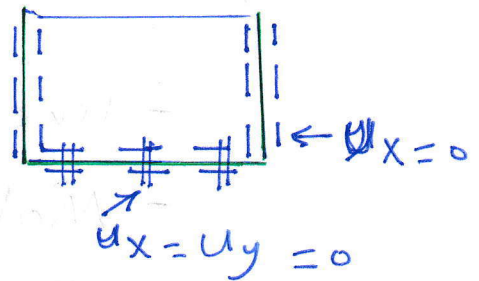
Stress (Gaussian element)

- 6-node element used for quick calculation for displacement ( $U_x, U_y$ ).

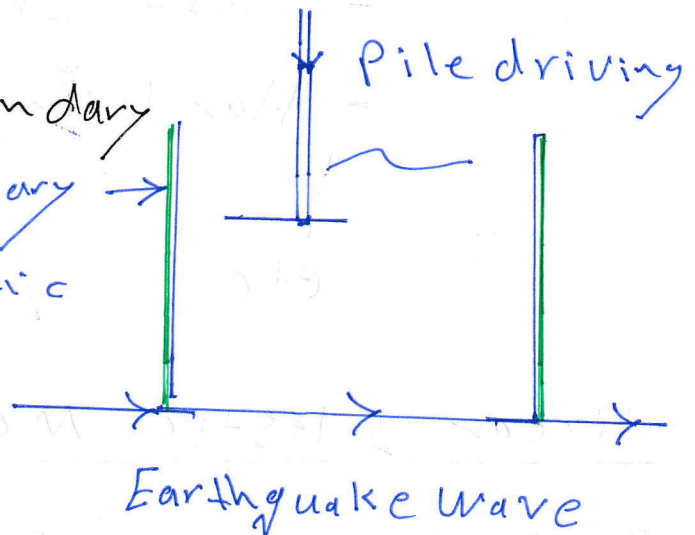
- 6-node element gives (3-stress) element for stress calculation.

## Boundary Condition

- Standard fixities boundary



- Absorbent boundary  
Absorbent boundary to prevent dynamic wave rebound (reflection)



## Material Sets

- Soil and Interfaces
- Plates
- Geogrids
- Anchors

## - Soil and Interfaces

### - Material Model

- linear Elastic

- Mohr-Coulomb

- Soft Soil Model

- Hardening

⋮

etc

### linear Elastic Model

Properties Required: ( $\gamma_{\text{unsat.}}$ ,  $\gamma_{\text{sat.}}$ ,

Permeability  $K_x, K_y$ , Modulus of Elasticity,

$E$ , Poisson's Ratio  $\nu$ ,

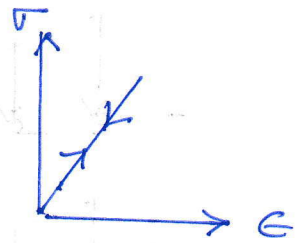
### Mohr Coulomb Model

In addition to above, Required  
the following properties:

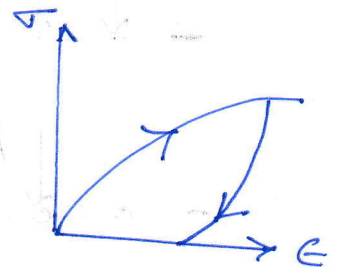
$c$  ( $\text{kN/m}^2$ ),  $\phi$  ( $^\circ$ )

## Plate Properties

- Elastic



- Elasto-Plastic



Properties Required:  $(EA \text{ (kN/m)}, EI \text{ (kN}\cdot\text{m}^2/\text{m)}, d \text{ (m)}, W \text{ (kN/m/m)})$

## Anchor Properties

- Elastic

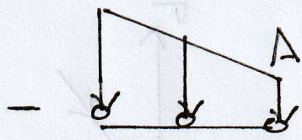
- Elasto-Plastic

Properties Required:  $(EA \text{ (kN)}, L \text{ spacing (m)})$

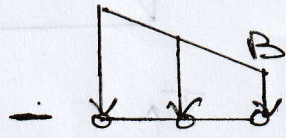
ملاحظة: يمكن تثبيت الرابطة  
Anchor أو Pile



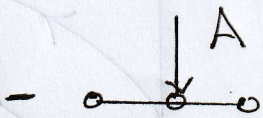
# Type of Load



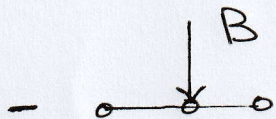
distributed Load - Load System A



distributed Load - Load system B

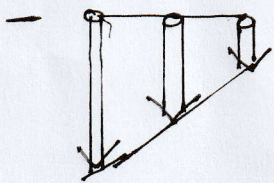


Point Load - Load System A



Point Load - Load System B

يمكن استخدام A أو B لكل نوع من Load وذلك لا ممانعة  
 استخدام احداهما في حالة Static والاخر في حالة Dynamic



Prescribed displacement

يقدم هذا الخيار في حالة تحليل dynamic

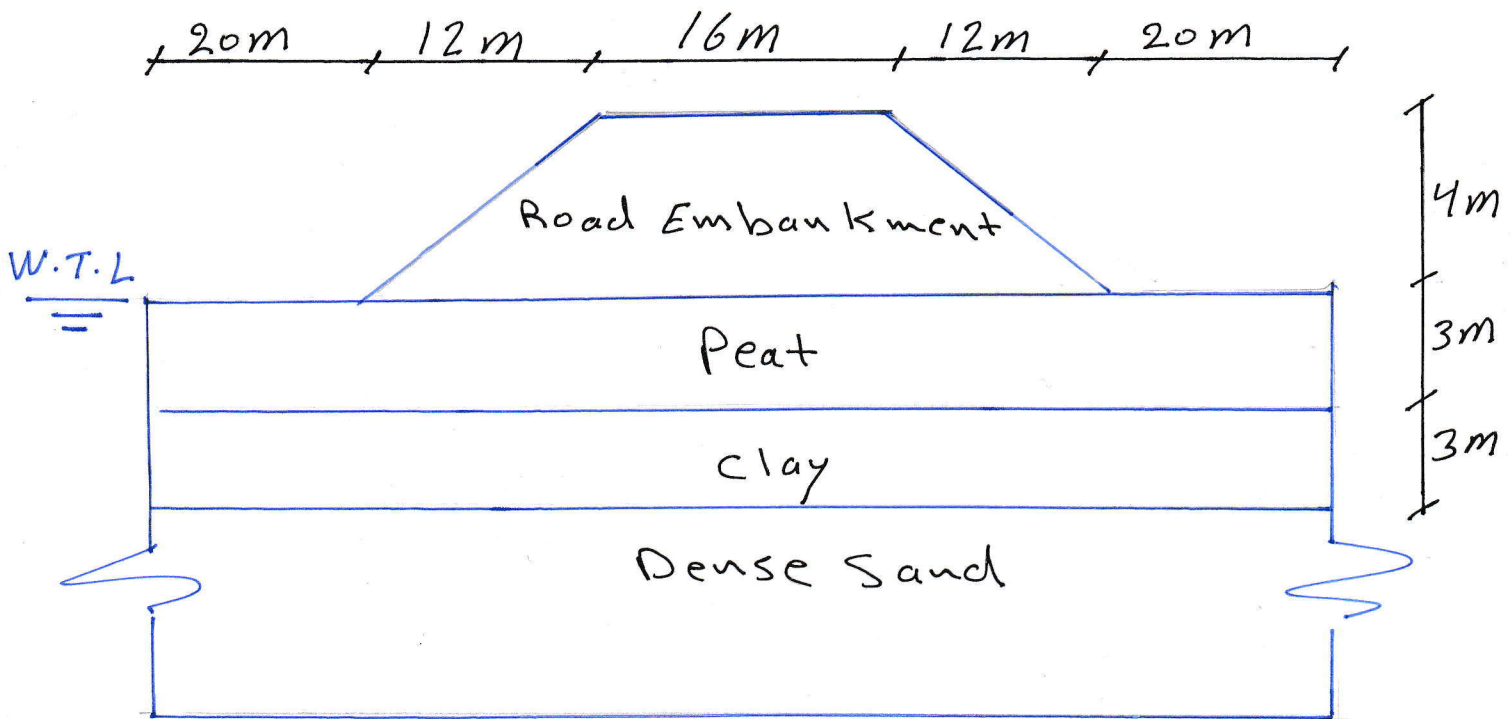
وخاصة عند تحليل Earthquake، حيث يتم استخدام  
 ازاحة ابتدائية عند الهبة الزلزالية في حالة Input وذلك  
 لتمثيل الموجة الزلزالية، وبعد ذلك يتم إجراء calculation  
 يتم ادخال الموجة الحقيقية اي الفترة الدورية.

من الممكن استخدام الينا لتحميل Static Load كما  
 في حالة تحميل Displacement وذلك وبمجرد الهبة الزلزالية

## Lesson 2:

### Construction of Road Embankment

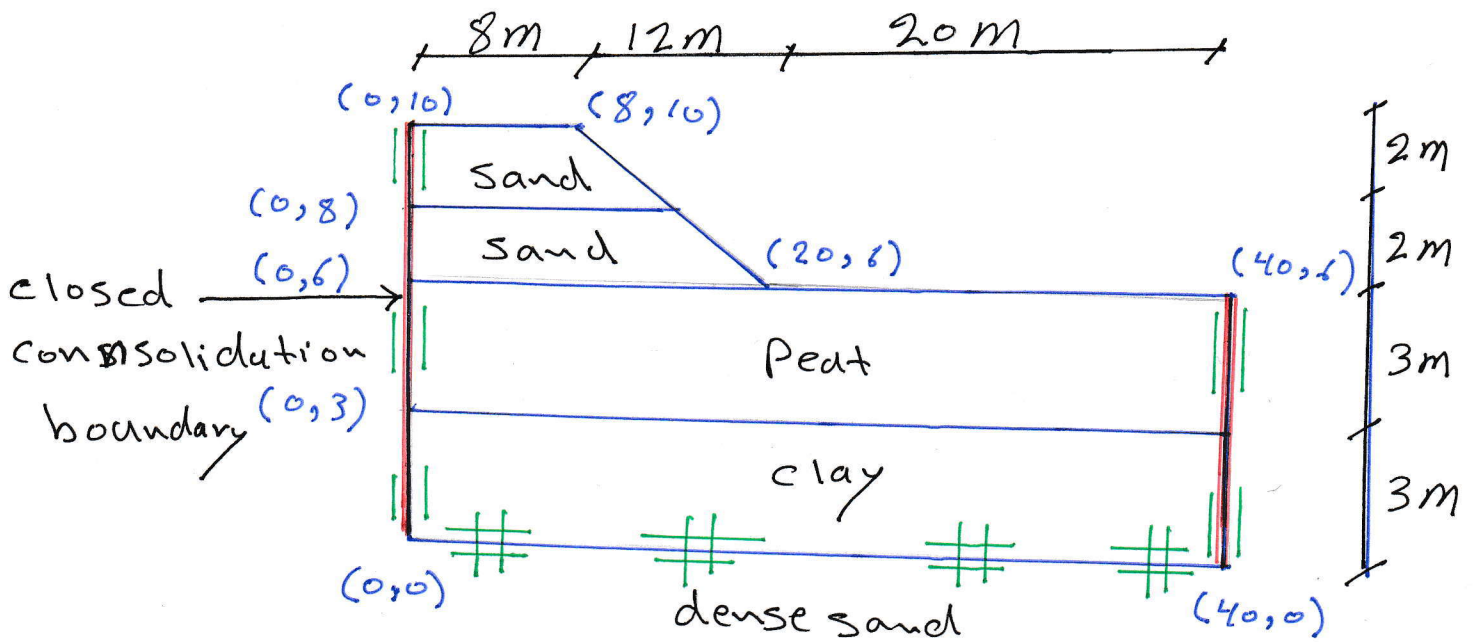
See Tutorial Manual (7-1 - 7-12)



Soils: 1- road embankment (loose sand)  
(16m x 4m thick) slope 1:3

2- 3.0 m soft soil layer (Peat) } sub-soil  
3- 3.0m clay }

4- Dense sand (continuous layer)



### Material Sets

Soil	clay	Peat	Sand
Model	MC	MC	MC
behaviours	undrained	undrained	drained
$\gamma_{uns.}$ ( $kN/m^3$ )	15	8	16
$\gamma_{sat}$ (below W.T)	18	11	20
$K_x$ (m/day)	$1 \times 10^{-4}$	$2 \times 10^{-3}$	1.0
$K_y$ (m/day)	$1 \times 10^{-4}$	$1 \times 10^{-3}$	1.0
$E$ ( $kN/m^2$ )	1000	350	3000
$\nu$	0.33	0.35	0.30
$C$ ( $kN/m^2$ )	20	5	1
$\phi^\circ$	24	20	30

clay and Peat are (undrained), this  
is because fast construction of  
embankment. This leads to grow  
the pore water pressure in this layer.

- Mesh generation
- Initial condition

W.T.L  $(0.0, 6.0)$ ,  $(40.0, 6.0)$

The water will be freely flow out  
the boundaries and excess pore pressure  
can dissipate in all direction.

In this problem:

The left vertical boundary must be  
closed, because this is a line of symmetry  
(H-flow should be not occur)

The right v. boundary should also  
be closed (no free flow  $\rightarrow$  this  
boundary

The bottom is open, permeable sand  
(not included in geometry)

The upper boundary is open as well

To do this:

use closed consolidation boundary |

### Calculation

- Phase 1: Consolidation

Time interval (5.0) days

Define Activate the first embank. layer

- Phase 2: Consolidation

Time interval (200) days

Activate the same first embank. layer

- Phase 3: Consolidation

Time interval (5.0) days

Define Activate the second embank. layer

- Phase 4: consolidation

Minimum Pore Pressure [P-stop]

$$\underline{1.0 \text{ kN/m}^2}$$

في هذا الطور Phase لا يتم كدب وقت الانتهاء كما في

الطور السابق، بل يتم كدب اقل  $1.0$  Pore Pressure

أي ان عملية الانتهاء تستمر كد الوصول الى اقل قيمة لضغط

الماء Pore Pressure (خروج جميع ماء الفجوات) وينتهي يتم الوصول

الى اقل Settlement في هذا الطور