

**College of Science  
Department of Physics  
Fourth Class  
Lecture 15**

**Quantum Mechanics**

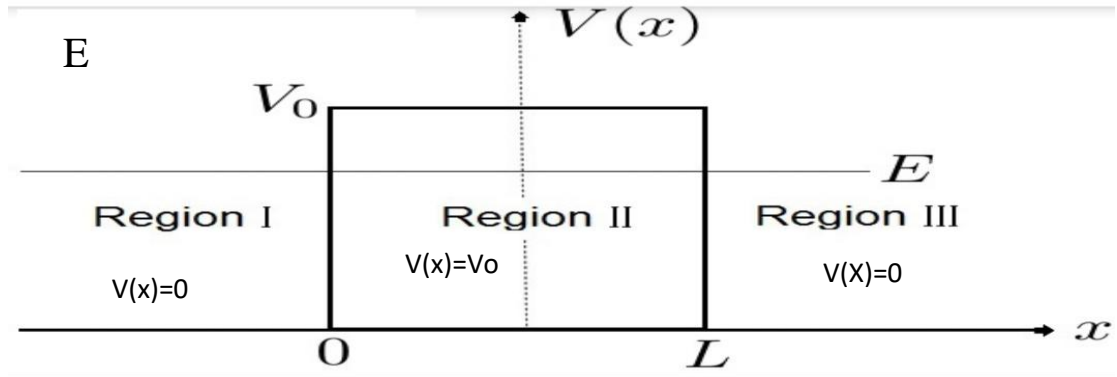
**2023-2024**

**Lecture 15: Rectangular potential barrier**

**Preparation**

**Assist. prof. Alaa Abdul Hakeim**

## 7.2 Rectangular potential barrier



$$V(x) = \begin{cases} 0 & \text{for } x < 0 \\ V_0 & \text{for } 0 < x < a \\ 0 & \text{for } x > a \end{cases} \quad \text{--- -- 33}$$

We have a potential barrier between  $x=0$  and  $x=a$ .

If a particle having energy less than  $V_0$  i.e.  $E < V_0$  approaches this barrier from left i.e. from region I, classically, the particle will always be reflected. However, quantum mechanics predicts that, the particle has some probability of penetrating to region III, the probability of penetrating being greater if  $(V_0 - E)$  and  $(a)$  are smaller. While if  $E > V_0$  classical mechanics predicts that the particle will always be transmitted, while according to wave mechanics the particle has a finite probability of transmission and hence it is not certain that the particle will penetrate the barrier. To solve the problem,

The schrödinger eq. for **region I** is

$$\frac{\partial^2 \psi_1}{\partial x^2} + \frac{2m}{\hbar^2} E \psi_1 = 0 \quad \text{--- -- 34}$$

The schrödinger eq. for **region II** is

$$\frac{\partial^2 \psi_2}{\partial x^2} + \frac{2m}{\hbar^2} (E - V_0) \psi_2 = 0 \quad \text{--- -- 35}$$

The schrödinger eq. for **region III** is

$$\frac{\partial^2 \psi_3}{\partial x^2} + \frac{2m}{\hbar^2} E \psi_3 = 0 \quad \text{--- -- 36}$$

$\Psi_1, \Psi_2$  and  $\Psi_3$  are wave functions for I, II, & III regions respectively .

The general solutions of eqs. (34,35,36) are

$$\Psi_1 = A_1 e^{\frac{iP_1x}{\hbar}} + B_1 e^{-\frac{iP_1x}{\hbar}} \text{ --- 37}$$

$$\Psi_2 = A_2 e^{\frac{iP_2x}{\hbar}} + B_2 e^{-\frac{iP_2x}{\hbar}} \text{ --- 38}$$

$$\Psi_3 = A_3 e^{\frac{iP_1x}{\hbar}} + B_3 e^{-\frac{iP_1x}{\hbar}} \text{ --- 39}$$

$P_1$  and  $P_2$  , the momenta of particles in the corresponding regions, are given by

$$P_1 = \sqrt{2mE} \quad , \quad P_2 = \sqrt{2m(E - V_0)} \text{ --- 40}$$

$A_1, B_1, A_2, B_2, A_3$  &  $B_3$  are constants to be determined by boundary conditions.

### **In eq. 37**

1<sup>st</sup> term represents the incident wave in region I and 2<sup>nd</sup> term represents the reflected wave in region I at  $x = 0$ .

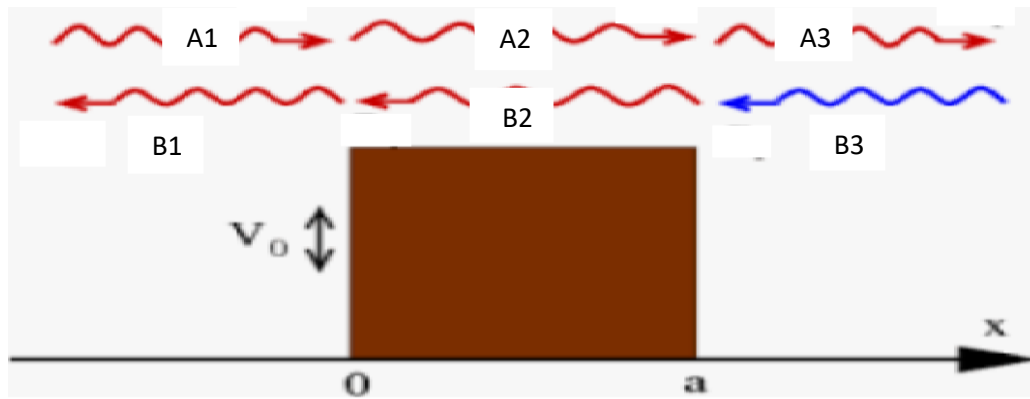
### **In eq. 38**

The 1<sup>st</sup> term represents the transmitted wave at  $x = 0$  in region II and 2<sup>nd</sup> term represents the reflected wave in region II at  $x = a$ .

### **In eq. 39**

The 1<sup>st</sup> term represents the transmitted wave into region III at  $x=a$  , but no wave travels back from infinity in region III. Consequently  $B_3=0$ , so that eq.39 can be written as

$$\Psi_3 = A_3 e^{\frac{iP_1x}{\hbar}} \text{ --- 41}$$



## Rectangular potential barrier ...

For evaluating the constants A1, B1, A2, B2 and A3 we shall apply the condition at two boundaries  $x = 0$  and  $x = a$ .

One condition is that  $\Psi$  must be continuous at the boundaries, i.e

$$\left. \begin{aligned} \Psi_1 &= \Psi_2 \text{ at } x = 0 \text{ --- (i)} \\ \Psi_2 &= \Psi_3 \text{ at } x = a \text{ --- (ii)} \end{aligned} \right\} \text{--- 42}$$

The other condition is that  $\frac{\partial \Psi}{\partial x}$  must be continuous at the boundaries.

$$\left. \begin{aligned} \frac{\partial \Psi_1}{\partial x} &= \frac{\partial \Psi_2}{\partial x} \text{ at } x = 0 \text{ --- (i)} \\ \frac{\partial \Psi_2}{\partial x} &= \frac{\partial \Psi_3}{\partial x} \text{ at } x = a \text{ --- (ii)} \end{aligned} \right\} \text{--- 43}$$

Applying boundary condition 42(i) to eq. 37 & 38 we have

$$A_1 + B_1 = A_2 + B_2 \text{ at } x=0 \text{ -----44}$$

Applying boundary condition 42(ii) to eqs.38&41 we get

$$A_2 e^{\frac{iP_2 a}{\hbar}} + B_2 e^{-\frac{iP_2 a}{\hbar}} = A_3 e^{\frac{iP_1 a}{\hbar}} \text{ at } x = a \text{ --- 45}$$

Differentiating eqs. 37,38 & 41, we get

$$\frac{\partial \Psi_1}{\partial x} = \frac{iP_1}{\hbar} \left[ A_1 e^{\frac{iP_1 x}{\hbar}} - B_1 e^{-\frac{iP_1 x}{\hbar}} \right] \text{ --- 46}$$

$$\frac{\partial \Psi_2}{\partial x} = \frac{iP_2}{\hbar} \left[ A_2 e^{\frac{iP_2 x}{\hbar}} - B_2 e^{-\frac{iP_2 x}{\hbar}} \right] \text{ --- 47}$$

$$\frac{\partial \Psi_3}{\partial x} = \frac{iP_1}{\hbar} \left[ A_3 e^{\frac{iP_1 x}{\hbar}} \right] \text{ --- 48}$$

Applying the boundary condition 43(i) & (ii) to these eqs., we get

$$P_1[A_1 - B_1] = P_2[A_2 - B_2] \quad \text{at } x = 0$$

$$\text{And } P_2 \left[ A_2 e^{\frac{iP_2 a}{\hbar}} - B_2 e^{-\frac{iP_2 a}{\hbar}} \right] = P_1 \left[ A_3 e^{\frac{iP_1 a}{\hbar}} \right] \quad \text{--- } x = a$$

$$\text{Or} \quad A_1 - B_1 = \frac{P_2}{P_1} (A_2 - B_2) \quad \text{--- } 49$$

$$A_2 e^{\frac{iP_2 a}{\hbar}} - B_2 e^{-\frac{iP_2 a}{\hbar}} = \frac{P_1}{P_2} A_3 e^{\frac{iP_1 a}{\hbar}} \quad \text{--- } 50$$

Solving eqs.44 & 49 for  $A_1$  &  $B_1$ , we get

$$A_1 = \frac{A_2}{2} \left( 1 + \frac{P_2}{P_1} \right) + \frac{B_2}{2} \left( 1 - \frac{P_2}{P_1} \right) \quad \text{--- } 51$$

$$B_1 = \frac{A_2}{2} \left( 1 - \frac{P_2}{P_1} \right) + \frac{B_2}{2} \left( 1 + \frac{P_2}{P_1} \right) \quad \text{--- } 52$$

Solving eqs.45 & 50 for  $A_2$  &  $B_2$  we get

$$A_2 = \frac{A_3}{2} \left( 1 + \frac{P_1}{P_2} \right) e^{\frac{i(P_1 - P_2)a}{\hbar}} \quad \text{--- } 53$$

$$B_2 = \frac{A_3}{2} \left( 1 - \frac{P_1}{P_2} \right) e^{\frac{i(P_1 + P_2)a}{\hbar}} \quad \text{--- } 54$$

Substituting values of  $A_2$  &  $B_2$  from these eqs. Into eqs.51 & 52, we get

$$A_1 = \frac{A_3}{4} e^{\frac{iP_1 a}{\hbar}} \left[ \left( 1 + \frac{P_2}{P_1} \right) \left( 1 + \frac{P_1}{P_2} \right) e^{-\frac{iP_2 a}{\hbar}} + \left( 1 - \frac{P_2}{P_1} \right) \left( 1 - \frac{P_1}{P_2} \right) e^{\frac{iP_2 a}{\hbar}} \right] \quad 55$$

$$B_1 = \frac{A_3}{4} e^{\frac{iP_1 a}{\hbar}} \left[ \left( 1 - \frac{P_2}{P_1} \right) \left( 1 + \frac{P_1}{P_2} \right) e^{-\frac{iP_2 a}{\hbar}} + \left( 1 + \frac{P_2}{P_1} \right) \left( 1 - \frac{P_1}{P_2} \right) e^{\frac{iP_2 a}{\hbar}} \right] \quad 56$$

Eq.55 may be written as

$$\frac{A_3}{A_1} = \frac{4e^{-\frac{iP_1 a}{\hbar}}}{\left[ \left( 1 + \frac{P_2}{P_1} \right) \left( 1 + \frac{P_1}{P_2} \right) e^{-\frac{iP_2 a}{\hbar}} + \left( 1 - \frac{P_2}{P_1} \right) \left( 1 - \frac{P_1}{P_2} \right) e^{\frac{iP_2 a}{\hbar}} \right]}$$

$$\frac{A_3}{A_1} = \frac{2P_1P_2 e^{\frac{-iP_1a}{\hbar}}}{(P_1^2 + P_2^2) \sinh\left(\frac{iP_2a}{\hbar}\right) + 2P_1P_2 \cosh\left(\frac{iP_2a}{\hbar}\right)}$$

$$\frac{A_3}{A_1} = \frac{2P_1P_2 e^{\frac{-iP_1a}{\hbar}}}{[(P_1^2 + P_2^2) \tanh\left(\frac{iP_2a}{\hbar}\right) + 2P_1P_2] \cosh\left(\frac{iP_2a}{\hbar}\right)}$$

$$\frac{A_3}{A_1} = \frac{2P_1P_2 \operatorname{sech}\left(\frac{iP_2a}{\hbar}\right) e^{\frac{-iP_1a}{\hbar}}}{[(P_1^2 + P_2^2) \tanh\left(\frac{iP_2a}{\hbar}\right) + 2P_1P_2]} \quad \text{--- -- 57}$$

The complex conjugate of above eq. is written as

$$\frac{A_3^*}{A_1^*} = \frac{2P_1P_2^* \operatorname{sech}\left(\frac{-iP_2^*a}{\hbar}\right) e^{\frac{+iP_1a}{\hbar}}}{[(P_1^2 + P_2^{*2}) \tanh\left(\frac{-iP_2^*a}{\hbar}\right) + 2P_1P_2^*]} \quad \text{--- -- 58}$$

Here  $P_2 = \sqrt{2m(E - V_o)}$  is imaginary since  $E < V_o$ , therefore  $iP_2$  is real, Since

$$P_2 = \sqrt{2m(E - V_o)} = \sqrt{-2m(V_o - E)} = i\sqrt{2m(V_o - E)}$$

so that we have

$$P_2^* = -i\sqrt{2m(V_o - E)} = -P_2$$

$$\therefore P_2^{*2} = P_2^2$$

Then eq.58 becomes

$$\frac{A_3^*}{A_1^*} = \frac{-2P_1P_2 \operatorname{sech}\left(\frac{iP_2a}{\hbar}\right) e^{\frac{+iP_1a}{\hbar}}}{[(P_1^2 + P_2^2) \tanh\left(\frac{iP_2a}{\hbar}\right) - 2P_1P_2]}$$

The transmittance or the transmission coefficient is given by

$$T = \frac{\text{magnitude of transmitted current}}{\text{magnitude of incident current}}$$

$$T = \frac{(A_3 A_3^*) \frac{P_1}{m}}{(A_1 A_1^*) \frac{P_1}{m}} = \frac{(A_3 A_3^*)}{(A_1 A_1^*)}$$

Using eq.57 & 59

$$T = \frac{\left[ 2P_1 P_2 \operatorname{sech} \left( \frac{iP_2 a}{\hbar} \right) e^{\frac{-iP_1 a}{\hbar}} \right] \left[ -2P_1 P_2 \operatorname{sech} \left( \frac{iP_2 a}{\hbar} \right) e^{\frac{+iP_1 a}{\hbar}} \right]}{\left[ (P_1^2 + P_2^2) \tanh \left( \frac{iP_2 a}{\hbar} \right) + 2P_1 P_2 \right] \left[ (P_1^2 + P_2^2) \tanh \left( \frac{iP_2 a}{\hbar} \right) - 2P_1 P_2 \right]}$$

Or

$$T = \frac{-4P_1^2 P_2^2 \operatorname{sech}^2 \left( \frac{iP_2 a}{\hbar} \right)}{(P_1^2 + P_2^2)^2 \tanh^2 \left( \frac{iP_2 a}{\hbar} \right) - 4P_1^2 P_2^2} \text{-----60}$$

Here  $P_2$  is imaginary, i.e.  $iP_2$  is real and so  $P_2^2$  is real therefore T is real.

The reflectance of the barrier or the reflected coefficient is given by

$$R = \frac{\text{magnitude of reflected current}}{\text{magnitude of incident current}}$$

$$R = \frac{B_1 B_1^*}{A_1 A_1^*} \text{-----61}$$

Using eqs.55 and 56 and remembering the  $P_2^* = -P_2$  eq.61, after simplification yield

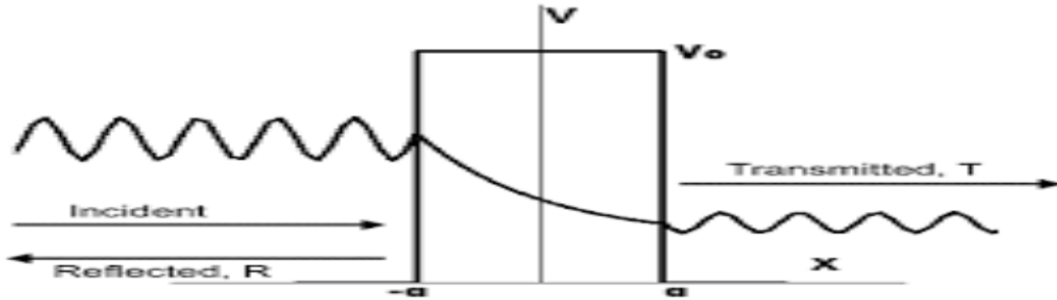
$$R = \frac{(P_1^2 - P_2^2)^2 \tanh^2 \left( \frac{iP_2 a}{\hbar} \right)}{(P_1^2 + P_2^2)^2 \tanh^2 \left( \frac{iP_2 a}{\hbar} \right) - 4P_1^2 P_2^2} \text{-----62}$$

The reflection coefficient R may be obtained by the fact

$$R + T = 1 \quad \text{i.e. } R = 1 - T \text{-----63}$$

The property of the barrier penetration is entirely due to the wave nature of matter and is very similar to the total internal reflection of light waves. If two plates of glass are placed close to each other with a layer of air as a medium between them, the light will be transmitted from one plate to

another, even though the angle of incident is greater than the critical angle. However, the intensity of transmitted wave will decrease exponentially with thickness of the layer of air. In this case the intensity of electron waves decreases exponentially with the thickness of the barrier. The wave function has the form "more or less" as shown in Fig



Let us consider a special case when the barrier is thick i.e.  $iP_2a > \hbar$  as (a) is very large or  $V_0 > E$

In this case  $\tanh\left(\frac{iP_2a}{\hbar}\right) = 1$  &  $\text{sech}\left(\frac{iP_2a}{\hbar}\right) = 2e^{\frac{iP_2a}{\hbar}}$

It is to be noted that  $P_2$  is imaginary and so  $iP_2$  and  $P_2^2$  are real and negative than eq.60 yield

$$T = \frac{-16P_1^2P_2^2e^{\frac{2iP_2a}{\hbar}}}{(P_1^2 + P_2^2)^2 - 4P_1^2P_2^2}$$

Or 
$$T = \frac{-16P_1^2P_2^2e^{\frac{2iP_2a}{\hbar}}}{(P_1^2 - P_2^2)^2} \text{----- 64}$$

And substituting values of  $P_1 = \sqrt{2mE}$  ,  $P_2 = \sqrt{2m(E - V_0)}$

In eq.64 gives

$$T = \frac{-16(2mE)2m(E - V_0)\exp\left(2i\sqrt{\frac{2m(E - V_0)}{\hbar^2}}a\right)}{[2mE - 2m(E - V_0)]^2}$$

$$T = \frac{16E(V_0 - E)}{V_0^2} \exp\left[-2\sqrt{\frac{2m(V_0 - E)}{\hbar^2}}a\right] \text{----- 65}$$



This is the expression for transmission coefficient for a very large barrier. The phenomenon of the particles (electrons, ray) penetrating the potential barrier is called "tunnel effect" and is especially important in thermionic and field emission

